Calculated Line Strengths for the Transition Array $(3d^3 + 3d^2 4s) - 3d^2 4p$ in Ti

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The transition array for the transitions between the configurations $(3d^3+3d^24s)$ and $3d^24p$ in Ti II are presented here. The relative line strengths have been calculated in the intermediate coupling scheme, taking into account interaction between configurations. The relative phase and magnitude of the radial transition integrals (s-p) and (d-p) for the jumping electron in the LS coupling have been determined empirically.

Key Words: Calculated line strengths; configuration interaction; intermediate coupling; Ti II; $3d^3$, $3d^24s$, $3d^24p$ configurations; transition array.

The line strengths for transitions between levels A and B are defined as in Condon and Shortley [1] as

$$\mathfrak{S}(A,B) = \sum_{a,b} |(a|\mathbf{P}|b)|^2, \tag{1}$$

where the sum is over all the states which are the sublevels of the levels A and B. In this note, we first calculated the square roots of the relative strengths of the transitions between two given configurations in the LS representation and then transformed to the physical representation. It is assumed that the dipole approximation is valid. In this approximation the transition operator \mathbf{P} is given by

$$\mathbf{P} = -\sum_{j} e \,\mathbf{r}_{j} \tag{2}$$

where the sum is taken over all the electrons involved in the transition. The matrix elements for the transition can be readily calculated except for a radial integral factor common to all the matrix elements of the transition array [2, 3].

The radial integral depends upon the quantum numbers of the jumping electron in the upper and lower levels of the transition. In cases where the interaction between configurations is negligible, one has only one radial integral to consider in the *LS* representation. Therefore, upon transforming to the intermediate coupling scheme, the relative transition strengths are easily obtained. However, in the case of Ti II, the interaction between the configurations is important, so one has to consider more than one radial integral for the jumping electron. In Ti II, transitions between the following configurations may be important:

(1)
$$3d^3 - 3d^24p$$
,

(2)
$$3d^24s - 3d^24p$$
.

The state $|a\rangle$ may then be expressed as a superposition of the eigenstates $|K\rangle$ of the various configurations. Thus,

$$|a\rangle = \sum_{K} |K\rangle (K|a), \qquad (3)$$

where we have summed over the configurations K, and (K|a) is the set of expansion coefficients. The matrix element of the transition between states a and b can be written as

$$(b | \mathbf{P} | a) = \sum_{K} \sum_{K'} (b | K') (K' | \mathbf{P} | K) (K | a), \qquad (4)$$

where $(K'|\mathbf{P}|K)$ are the matrix elements of the transition operator \mathbf{P} expressed in the representation where the configurations K' and K are good quantum

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numbers. In Ti II, this refers to the transition array in the LS representation for each configuration of the lower state separately. The matrix element for the transition can then be expressed as

$$(b|\mathbf{P}|a) = \sum_{\substack{\alpha \\ \beta}} (a|3d^{2}4p, \beta) (3d^{2}4p\beta|\mathbf{P}|3d^{3}, \alpha)(3d^{3}, \alpha|a)$$

$$+ \sum_{\substack{\alpha' \\ \beta'}} (b|3d^{2}4p\beta')(3d^{2}4p\beta'|\mathbf{P}|3d^{2}4s\alpha')$$

$$(3d^{2}4s, \alpha'|a) \qquad (5)$$

where α , α' and β , β' are the sets of relevant quantum numbers in the LS representation. In each of the two sums in eq (5) there is a factorable radial integral factor $(nl\|P\|n'l')$, where nl and n'l' are the radial and orbital angular momentum quantum numbers of the jumping electron. Each set of configurations has a different set of n, l; n', l'. It is the phase and magnitude of the ratio of these radial factors which must be determined to calculate the relative intensities.

The determination of the expansion coefficients (K|a) and the relative phase and magnitude as well

as comparison with experiments are discussed elsewhere [4]. In the table we show the strengths for the transition array for $3d^3 + 3d^24s - 3d^24p$ for Ti II. The composition of the upper and lower level is described in terms of the dominant states in the LS representation. For each position in the array, the upper number is the relative strength of the transition. The next lower number is the wavelength corresponding to the transition obtained from Russell's classifications [5], whenever available. The lowest number gives the wavenumber corresponding to the transition. The relative strengths are given to three significant figures for the stronger transitions and only one significant figure for the weaker lines. The number of significant figures given is consistent with the results of the diagonalization of the energy matrix and the empirical determination of the ratio of the radial integral parameters [4]. The magnitudes of the radial integral parameters have been found to be equal within the approximations that have been used, so in this table, the magnitudes of the radial integral factor have been taken to be unity for simplicity. Those relative strengths listed as zero indicate that, on the scale employed here, these strengths are less than 5×10^{-5} .

Table 1. Transition array for $(3d^3 + 3d^24s) - 3d^24p$ in Ti II in intermediate coupling scheme with configuration interaction.

The upper and lower levels are described in terms of the dominant states in the LS representation and the energy levels assigned in AEL [6]. For each position in the array, the upper number is the relative strength of the transition with the normalization of the radial integral parameter for the jumping electron in the d-p transition taken as unity. The next lower number is the wavelength corresponding to the transition obtained from Russell's classification when available. The lowest number is the wave number of the transition.

 $(3d^3 + 3d^24s)$

1/2	a ² P 9850.90	a ⁴ P 9363.71	a^2 S 21338.0	<i>b</i> ² P 16515.79	<i>b</i> ⁴ P 9872.87
z ² S° 37430.55	0.0004 3624.82 27579.65	0.0000 3561.92 28066.84	0.0000 6212.29 16092.55	0.30 4779.95 20914.76	0.0001 3627.70 27557.68
2P°	0.0003	0.0000	0.66	0.003	0.0000
(63210.1)	53359.20	53846.39	41872.10	46694.31	53337.23
y²P°	0.21	0.02	0.004	0.23	0.003
45472.89	2806.50 35621.99	36109.18	24134.89	3452.47 28957.10	35600.02
z²P°	0.06 3352.06	0.003 3298.20	0.005 5452.02	0.02 4316.80	0.002
39674.64	29823.74	30310.93	18336.64	23158.85	29801.77
z ⁴ P°	0.003	0.01 3063.48	0.0000 4839.22	0.0001	0.10 3112.05
41996.74	32145.84	32633.03	20658.74	25480.95	32123.87
y ⁴ D°	0.005	0.01	0.0000	0.0000	0.55
40330.25	30479.35	30966.54	18992.25	23814.46	3282.33 30457.38
z ⁴ D°	0.007	0.08	0.0000	0.0000	0.008
	4407.68	4314.98			4411.94

 $(3d^24p)$

32532.38

22681.48

23168.67

11194.38

16016.59

22659.51

TABLE 1. - Continued

	3/2	$a^2\mathrm{P}$	a4P	$d_1^2\mathrm{D}$	$b_3^2\mathrm{D}$	b⁴F	b ² P	b ⁴ P	$a^2\mathrm{D}$	a4F	D ² D
	1/2	9975.92	9395.76	(32358.5)	12628.77	907.96	16625.25	9930.74	8710.47	0	24961.34
	z ² S° 37430.55	0.26 3641.33 27454.63	0.04 3566.00 28034.79	0.0000 5072.05	0.002 24801.78	0.0000 36522.59	0.18 4805.10 20805.30	0.03 27499.81	0.02 3480.89 28720.08	0.0000 37430.55	0.0001 12469.21
	² P°	0.0008	0.0001	0.14	0.03	0.0000	0.002	0.0001	0.0002	0.0000	0.02
	(63210.1)	53234.18	53814.34	30851.60	50581.33	62302.14	46584.85	53279.36	54499.63	63210.10	38248.76
10.4	y ² P° 45472.89	0.01 35496.97	0.002 36077.13	0.14 13114.39	0.06 3043.85 32844.12	0.0000 44564.93	0.22 3465.58 28847.64	0.002 35542.15	0.001 2719.39 36762.42	0.0000 45472.89	0.04 4873.95 20511.55
² 4p)	z ² P° 39674.64	0.09 3366.17 29698.72	0.02 30278.88	0.0008 7316.14	0.002 3696.38 27045.87	0.0001 38766.68	0.002 4337.32 23049.39	0.01 29743.90	0.69 3228.60 30964.17	0.0003 39674.64	0.008 14713.30
	z ⁴ P° 41996.74	0.02 3122.10 32020.82	0.07 3066.52 32600.98	0.0000 9638.24	0.0001 29367.97	0.0000 41088.78	0.0001 25371.49	0.54 3117.67 32066.00	0.0000 33286.27	0.0000 41996.74	0.0000 17035.40
	y ⁴ D° 40330.25	0.01 30354.33	0.002 30934.49	0.0000 7971.75	0.0000 27701.48	0.08 2535.87 39422.29	0.0001 23705.00	0.09 3288.58 30399.51	0.0008 31619.78	0.01 2478.77 40330.25	0.0000 15368.91
	z ⁴ D° 32532.38	0.0005 4432.10 22556.46	0.02 4320.95 23136.62	0.0000 173.88	0.0000 19903.61	0.16 3161.20 31624.42	0.0000 15907.13	0.002 22601.64	0.0000 23821.91	0.66 3072.97 32532.38	0.0000

TABLE 1.—Continued

1/2	a^2 P	$a^4\mathrm{P}$	$a^2\mathrm{S}$	$b^2\mathrm{P}$	$b^4\mathrm{P}$
3/2	9850.90	9363.71	21338.0	16515.79	9872.87
z ⁴ S°	0.03	0.09	0.0005	0.0006	0.20
40027.28	30176.38	3260.26 30663.57	18689.28	23511.49	3315.32 30154.41
2P°	0.0006	0.0000	1.32	0.0007	0.0000
(63284.3)	53433.40	53920.59	41946.30	46768.51	53411.43
y ² P°	0.007	0.0006	0.007	0.14	0.0000
45548.90	35698.00	36185.19	24210.90	3443.38 29033.11	35676.03
$z^2\mathrm{P}^\circ$	0.04	0.02	0.01	0.002	0.01
39602.90	29752.00	3306.04 30239.19	5473.52 18264.90	4330.25 23087.11	3362.66 29730.03
z ⁴ P°	0.0008	0.07	0.0001	0.0001	0.52
42068.85	3103.00 32217.95	3056.74 32705.14	20730.85	25553.06	3105.08 32195.98
x2D°	0.13	0.01	0.0001	0.86	0.001
44914.80	2851.10 35063.90	2812.05 35551.09	23576.80	3520.25 28399.01	35041.93
y ² D°	0.05	0.004	0.0003	0.05	0.008
39233.44	3402.42 29382.54	29869.73	17895.44	22717.65	3404.99 29360.57
$z^2\mathrm{D}^\circ$	0.18	0.03	0.0000	0.01	0.0004
31756.50	4563.77 21905.60	4464.47 22392.79	10418.50	6559.58 15240.71	4568.30 21883.63
y⁴D°	0.02	0.005	0.0000	0.001	0.56
40425.80	3269.75 30574.90	31062.09	19087.80	23910.01	3272.08 30552.93
z ⁴ D°	0.03	0.06	0.0000	0.0006	0.01
32602.51	4394.06 22751.61	4301.93 23238.80	11264.51	16086.72	4398.31 22729.64
z ⁴ F°	0.0003	0.0000	0.0000	0.0000	0.0000
30836.52	20985.62	21472.81	9498.52	14320.73	20963.65

 $(3d^3 + 3d^24s)$

3/2	a ² P 9975.92	a ⁴ P 9395.76	d_1^2 D (32358.5)	b_3^2 D 12628.77	<i>b</i> ⁴ F 907.96	<i>b</i> ² P 16625.25	<i>b</i> ⁴ P 9930.74	a^{2} D 8710.47	a ⁴ F 0	C ² D 24961.34
z ⁴ S° 40027.28	0.0004 30051.36	0.18 3263.68 30631.52	0.0002 7668.78	0.005 27398.51	0.0000 39119.32	0.007 23402.03	0.52 3321,70 30096.54	0.009 3192.26 31316.81	0.0000 40027.28	0.0000 15065.94
² P° (63284.3)	0.0003	0.0000	0.03	0.003	0.0000 62376.34	0.008	0.0000	0.004 54573.83	0.0000	0.004
y ² P° 45548.90	0.50 35572.98	0.06 2765.22 36153.14	0.04	0.02 3036.78 32920.13	0.0000	0.63 3456.39 28923.65	0.08	0.001 2713.76 36838.43	0.0000 45548.90	0.01 20587.56
z ² P° 39602.90	0.12 3374.35 29626.98	0.05	0.0001 7244.40	0.07 3706.23 26974.13	0.0000 38694.94	0.06 4350.83 22977.65	0.002 3369.20 29672.16	0.002 3236.12 30892.43	0.0001 39602.90	0.0000 14641.56
z ⁴ P° 42068.85	0.04 3115.09 32092.93	0.02 3059.74 32673.09	0.0000 9710.35	0.0001 29440.08	0.0000 41160.89	0.0002 25443.60	0.14 3110.67 32138.11	0.0000 33358.38	0.0000 42068.85	0.0000 17107.51
x ² D° 44914.80	0.03 2861.29 34938.88	0.007 2814.61 35519.04	0.06 12556.30	0.0005 3096.43 32286.03	0.0000 44006.84	0.07 3533.85 28289.55	0.008 34984.06	0.16 2761.29 36204.33	0.0000 44914.80	0.02 5010.21 19953.46
y ² D° 39233.44	0.03 3416.95 29257.52	0.02 3350.53 29837.68	0.02 6874.94	0.008 3757.69 26604.67	0.0008 38325.48	0.04 4421.95 22608.19	0.01 29302.70	1.19 3275.38 30522.97	0.0000 39233.44	0.004 14272.10
z ² D° 31756.50	0.002 4589.95 21780.58	0.01 4470.88 22360.74	0.01	0.18 5226.56 19127.73	0.001 3240.72 30848.54	0.04 15131.25	0.001 4580.46 21825.76	0.002 4337.92 23046.03	0.03 3148.04 31756.50	0.0004 6795.16
y ⁴ D° 40425.80	0.07 30449.88	0.009 31030.04	0.0008 8067.30	0.0001 3596.55 27797.03	0.03 2529.86 39517.84	0.001 23800.55	0.57 3278.29 30495.06	0.02 31715.33	0.004 40425.80	0.0001 15464.46
z ⁴ D° 32602.51	0.02 4418.33 22626.59	0.09 4307.90 23206.75	0.0008 244.01	0.009 19973.74	0.07 3154.20 31694.55	0.002 15977.26	0.004 4409.53 22671.77	0.0001 4184.33 23892.04	0.23 3066.36 32602.51	0.0000 7641.17
z ⁴ F° 30836.52	0.0000 20860.60	0.0000 21440.76	0.0001	0.0003 18207.75	0.32 3340.34 29928.56	0.0001 14211.27	0.0000 20905.78	0.0000 22126.05	1.07 3241.99 30836.52	0.0000 5875.18

TABLE 1.—Continued

3/2	$a^2\mathrm{P}$	a4P	$d_{1}^{2}\mathrm{D}$	$b_3^2\mathrm{D}$	b⁴F	b ² P	b⁴P	$a^2\mathrm{D}$	a⁴F	C2D
5/2	9975.92	9395.76	(32358.5)	12628.77	907.96	16625.25	9930.74	8710.47	0	24961.34
z ⁴ P°	0.02	0.07	0.0000	0.001	0.0000	0.001	0.55 3097.19	0.0000	0.0000	0.0000
42208.84	32232.92	3046.69 32813.08	9850.34	29580.07	41300.88	25583.59	32278.10	33498.37	42208.84	17247.50
x2D°	0.19 2862.32	0.02 2815.57	0.01	0.02 3097.63	0.0000	1.39 3535.41	0.03	0.02 2762.22	0.0000	0.002
44902.42	34926.50	35506.66	12543.92	32273.65	43994.46	28277.17	34971.68	36191.95	44902.42	19941.08
y²D°	0.07	0.04	0.001	0.10	0.0001	0.07	0.10	0.11	0.0000	0.002
39476.87	3388.76 29500.95	30081.11	7118.37	3723.60 26848.10	38568.91	4374.82 22851.62	29546.13	3249.37 30766.40	39476.87	14515.53
$z^2\mathrm{D}^\circ$	0.24	0.13	0.004	0.02	0.0003	0.02	0.02	0.006	0.003	0.0000
32025.50	4533.97 22049.58	4417.72 22629.74		5154.07 19396.73	31117.54	6491.68 15400.25	4524.72 22094.76	4287.88 23315.03	3121.60 32025.50	7064.16
y ⁴ D°	0.28	0.005	0.0000	0.0000	0.002	0.004	1.11	0.0000	0.0003	0.0000
40581.80	3266.41 30605.88	31186.04	8223.30	3576.37 27953.03	2519.79 39673.84	23956.55	3261.59 30651.06	3136.75 31871.33	40581.80	15620.46
z ⁴ D°	0.08	0.12	0.0003	0.002	0.005	0.003	0.06	0.0004	0.01	0.0000
32697.94	4399.77 22722.02	4290.23 23302.18	339.44	20069.17	31789.98	16072.69	4391.02 22767.20	23987.47	3057.40 32697.94	7736.60
y²F°	0.01 3337.79	0.005	0.003	0.23 3662.24	0.0001	0.001	0.001	1.35 3202.54	0.0000	0.02 6680.26
39926.83	29950.91	30531.07	7568.33	27298.06	39018.87	23301.58	29996.09	31216.36	39926.83	14965.49
$z^2\mathrm{F}^\circ$	0.002	0.0001	0.02	0.02	0.005	0.0005	0.0000	0.21	0.0000	0.0001
31207.44	4708.65 21231.52	4583.44 21811.68		5381.02 18578.67	30299.48	14582.19	21276.70	4443.80 22496.97	3203.44 31207.44	6246.10
x^2F°	0.0003	0.0002	0.20	0.03	0.0000	0.0006	0.0001	0.009	0.0000	0.04
47625.17	2655.30 37649.25	38229.41	15266.67	2856.62 34996.40	46717.21	30999.92	37694.43	2568.98 38914.70	47625.17	4411.08 22663.83
z ⁴ F°	0.0001	0.0000	0.0007	0.001	0.08	0.0000	0.0001	0.007	0.26	0.0000
30958.70	20982.78	4636.34 21562.94		18329.93	3326.76 30050.74	14333.45	21027.96	4493.52 22248.23	3229.19 30958.70	5997.36
z4G°	0.0000	0.0000	0.0001	0.0000	0.06	0.0000	0.0000	0.001	1.72	0.0000
29544.37	19568.45	20148.61		16915.60	3491.05 28636.41	12919.12	19613.63	4798.52 20833.90	3383.76 29544.37	4583.03

TABLE 1.—Continued

5/2	$a^4\mathrm{P}$	$d^2\mathrm{D}$	$d_1^2\mathrm{D}$	$b^2\mathrm{F}$	$b^4\mathrm{F}$	b ⁴ P	$a^2\mathrm{D}$	$a^2\mathrm{F}$	$a^4\mathrm{F}$	C2D
3/2	9518.05	(32362.7)	12758.15	20951.77	983.80	10024.74	8744.27	4628.61	93.94	25193.04
z ⁴ S°	0.35	0.0000	0.0000	0.0000	0.0001	0.63	0.02	0.0002	0.0000	0.0008
40027.28	3276.76 30509.23	7664.58	27269.13	19075.51	39043.48	3332.11 30002.54	3195.71 31283.01	35398.67	39933.34	14834.24
²P°	0.0000	0.24	0.06	0.0000	0.0000	0.0000	0.0001	0.0000	0.0000	0.05
(63284.3)	53766.25	30921.60	50526.15	42332.53	62300.50	53259.56	54540.03	58655.69	63190.36	38091.26
y ² P°	0.0000	0.23	0.08	0.006	0.0000	0.0000	0.004	0.0003	0.0000	0.07
45548.90	36030.85	13186.20	3048.77 32790.75	4064.40 24597.13	44565.10	35524.16	2716.25 36804.63	40920.29	45454.96	4911.19 20355.86
z²P°	0.004	0.0008	0.008	0.0000	0.0001	0.007	1.41	0.003	0.0003	0.02
39602.90	30084.85	7240.20	3724.08 26844.75	18651.13	38619.10	3379.92 29578.16	3239.66 30858.63	2858.40 34974.29	39508.96	14409.86
z ⁴ P°	0.08	0.0000	0.001	0.0000	0.0000	0.64	0.0002	0.0001	0.0000	0.0001
42068.85	3071.24 32550.80	9706.15	29310.70	21117.08	41085.05	3119.80 32044.11	33324.58	37440.24	41974.91	16875.81
x ² D°	0.0000	0.02	0.02	0.62	0.0000	0.0001	0.009	0.04	0.0000	0.004
44914.80	35396.75	12552.10	3108.93 32156.65	4171.90 23963.03	43931.00	34890.06	36170.53	2481.49 40286.19	44820.86	5069.12 19721.76
γ²D°	0.003	0.0007	0.07	0.0004	0.005	0.0000	0.003	0.08	0.0005	0.0000
39233.44	29715.39	6870.74	3776.06 26475.29	18281.67	38249.64	3422.69 29208.70	3278.92 30489.17	2888.93 34604.83	39139.50	14040.40
z²D°	0.0004	0.002	0.008	0.01	0.01	0.0003	0.01	1.10	0.05	0.0000
31756.50	22238.45		5262.14 18998.35	10804.73	30772.70	21731.76	4344.29 23012.23	3685.19 27127.89	3157.39 31662.56	6563.46
y ⁴ D°	0.003	0.0000	0.003	0.0000	0.13	0.07	0.001	0.002	0.02	0.0000
40425.80	30907.75	8063.10	27667.65	19474.03	2534.62 39442.00	3288.42 30401.06	31681.53	35797.19	2478.64 40331.86	15232.76
z ⁴ D°	0.01	0.0001	0.0005	0.0005	0.23	0.0007	0.001	0.06	1.01	0.0000
32602.51	4330.71 23084.46	239.81	19844.36	11650.74	3161.77 31618.71	22577.77	4190.29 23858.24	3573.74 27973.90	3075.22 32508.57	7409.47
z ⁴ F°	0.0000	0.0000	0.0001	0.0000	0.08	0.0000	0.0000	0.003	0.26	0.0000
30836.52	21318.47		18078.37	9884.75	3348.82 29852.72	20811.78	22092.25	3814.57 26207.91	3251.91 30742.58	5643.48

TABLE 1.—Continued

5/2	a ⁴ P	$d_1^2\mathrm{D}$	$b_3^2\mathrm{D}$	b ² F	b⁴F	b ⁴ P	$a^2\mathrm{D}$	a ² F	a⁴F	C2D
5/2	9518.05	(32362.7)	12758.15	20951.77	983.80	10024.74	8744.27	4628.61	93.94	25193.04
z ⁴ P°	0.17 3058.09	0.0004	0.0006	0.0000	0.0000	1.45 3106.23	0.0002 2987.38	0.0000	0.0000	0.0000
42208.84	32690.79	9846.14	29450.69	21257.07	41225.04	32184.10	33464.57	37580.23	42114.90	17015.80
x ² D° 44902.42	0.0004 35384.37	0.10 12539.72	0.0009 3110.11 32144.27	0.04 23950.65	0.0000 43918.62	0.004 34877.68	0.26 2764.80 36158.15	0.009 40273.81	0.0000 44808.48	0.05 5072.30 19709.38
y ² D° 39476.87	0.001 336.98 29958.82	0.03 7114.17	0.0000 3741.64 26718.72	0.0000 18525.10	0.002 38493.07	0.02 29452.13	1.72 30732.60	0.0001 2868.74 34848.26	0.0001 39382.93	0.006 14283.83
z ² D° 32025.50	0.01 22507.45	0.02	0.22 5188.70 19267.35	0.0005 11073.73	0.007 3220.48 31041.70	0.0001 4544.01 22000.76	0.001 4294.12 23281.23	0.008 27396.89	0.06 3130.80 31931.56	0.0008 6832.46
y ⁴ D° 40581.80	0.01 31063.75	0.002 8219.10	0.001 3593.11 27823.65	0.0006 19630.03	0.04 2524.64 39598.00	0.53 3271.65 30557.06	0.07 31837.53	0.001 2780.55 35953.19	0.005 2409.13 40487.86	15388.76
z ⁴ D° 32697.94	0.08 4312.87 23179.89	0.003 335.24	0.03 5013.69 19939.79	0.0000 11746.17	0.08 3152.25 31714.14	0.01 4409.23 22673.20	0.0002 4173.55 23953.67	0.008 3561.59 28069.33	0.27 3066.22 32604.00	0.0001 7504.90
y ² F° 39926.83	0.0009 30408.78	0.004 7564.13	0.03 27168.68	0.08 5268.63 18975.06	0.0008 38943.03	0.002	0.21 3206.00 31182.56	0.12 2832.16 35298.22	0.0001 39832.89	0.0002 14733.79
z ² F°	0.0002	0.002	0.04 5418.77	0.12	0.02 3307.72	0.0000 4719.51	0.0008 4450.49	1.70 3761.32	0.05 3213.14	0.0002
31207.44	21689.39		18449.29	10255.67	30223.64	21182.70	22463.17	26578.83	31113.50	6014.40
x ² F° 47625.17	0.0000 38107.12	0.02 15262.47	0.0001 34867.02	0.26 3748.01 26673.40	0.0000 46641.37	0.0001 37600.43	0.002 38880.90	0.01 42996.56	0.0000 47531.23	0.005 4456.62 22432.13
z ⁴ F° 30958.70	0.0000 21440.65	0.0000	0.0004 18200.55	0.005 10006.93	0.39 3335.20 29974.90	0.0000 20933.96	0.0001 22214.43	0.05 3796.88 26330.09	1.36 3239.04 30864.72	0.0000 5765.66
z ⁴ G° 29544.37	0.0000	0.0000	0.0001 16786.22	0.0005 8592.60	0.01 3500.33 28560.57	0.0000 19519.63	0.0000	0.008 4012.39 24915.76	0.26 3394.58 29450.43	0.0000

TABLE 1.—Continued

5/2	a ⁴ P	$d_1^2\mathrm{D}$	$b_3^2\mathrm{D}$	$b^2\mathrm{F}$	b⁴F	b ⁴ P	$a^2\mathrm{D}$	$a^2\mathrm{F}$	a⁴F	C2D
7/2	9518.05	(32362.7)	12758.15	20951.77	983.80	10024.74	8744.27	4628.61	93.94	25193.04
у ⁴ D° 40798.37	0.04 3195.99 31280.32	0.0002 8435.67	0.02 3565.33 28040.22	0.0000 19846.60	0.002 2510.90 39814.57	2.59 3248.60 30773.63	0.01 3118.85 32054.10	0.0002 2763.90 36169.76	0.0002 40704.43	0.001 15605.33
z ⁴ D°	0.42	0.0000	0.0005	0.0000	0.004	0.04	0.001	0.0002	0.01	0.0000
32767.02	4300.05 23248.97	404.32	20008.87	11815.25	31783.22	4395.86 22742.28	4161.54 24022.75	28138.41	3059.73 32673.08	7573.98
y²F°	0.0005	0.005	0.33 3659.76	0.002	0.0001	0.03	2.07 3190.87	0.008	0.0001	0.03 6717.89
40074.71	30556.66	7712.01	27316.56	19122.94	39090.91	30049.97	31330.44	35446.10	39980.77	14881.67
$z^2 \mathrm{F}^\circ$	0.0002	0.03	0.04 5336.81	0.0003	0.004 3276.98	0.004 4657.20	0.33 4395.04	0.08 3721.64	0.0004 3184.09	0.0001
31490.82	21972.77		18732.67	10539.05	30507.02	21466.08	22746.55	26862.21	31396.88	6297.78
x ² F°	0.0002	0.28	0.05 2880.28	0.01 3770.40	0.0000	0.0002	0.01 2581.73	0.0000	0.0000	0.06 4488.32
47466.80	37948.75	15104.10	34708.65	26515.03	46483.00	37442.06	38722.53	42838.19	47372.86	22273.76
z ⁴ F°	0.0002	0.0007	0.001	0.0000	0.11 3318.03	0.0002	0.007 4469.15	0.004	0.33 3222.84	0.0000
31113.61	21595.56		18355.46	10161.84	30129.81	21088.87	22369.34	26485.00	31019.67	5920.57
$z^2 \mathrm{G}^\circ$	0.0000	0.0000	0.0001	0.03	0.0000	0.0000	0.0000	2.45 3341.88	0.0001 2901.94	0.0000
34543.36	25025.31	2180.66	21785.21	13591.59	33559.56	24518.62	25799.09	29914.75	34449.42	9350.32
y ² G°	0.0000	0.0000	0.0002	0.20 4386.86	0.0000	0.0000	0.0009	0.07 2555.99	0.0000	0.0000
43740.77	34222.72	11378.07	30982.62	22789.00	42756.97	33716.03	34996.50	39112.16	43646.83	18547.73
z ⁴ G°	0.0000	0.0000	0.0000	0.0000	0.07 3477.18	0.0000	0.0006 4762.78	0.0002 3982.01	2.32 3372.80	0.0000
29734.45	20216.40		16976.30	8782.68	28750.65	19709.71	20990.18	25105.84	29640.51	4541.41
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TABLE 1. - Continued

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	7/2	$b^2\mathrm{F}$	b⁴F	a^2 G	$a^2\mathrm{F}$	a⁴F	b ² G
	5/2	20891.88	1087.21	8997.69	4897.60	225.47	15265.60
	z ⁴ P°	0.0000	0.0001	0.0000	0.0007	0.0000	0.0000
	42208.84	21316.96	41121.63	33211.15	37311.24	41983.37	26943.24
	$x^2\mathrm{D}^\circ$	0.89	0.0000	0.0004	0.07	0.0000	0.0007
	44902.42	4163.65 24010.54	43815.21	35904.73	2498.94 40004.82	44676.95	29636.82
	y²D°	0.003	0.01 2604.11	0.009 3279.98	0.11 2891.07	0.001 2546.88	0.002
	39476.87	18584.99	38389.66	30479.18	34579.27	39251.40	24211.27
	$z^2\mathrm{D}^\circ$	0.01	0.05 3231.32	0.005 4341.39	1.52 3685.20	0.19 3143.76	0.0000
1	32025.50	11133.62	30938.29	23027.81	27127.90	31800.03	16759.90
	y⁴D°	0.0000	0.19	0.004	0.004	0.02	0.0007
	40581.80	19689.92	2531.25 39494.59	31584.11	35684.20	2477.21 40356.33	25316.20
	z ⁴ D°	0.002	0.33	0.0001	0.21	1.44	0.0000
	32697.94	11806.06	3162.57 31610.73	23700.25	3596.05 27800.34	3078.64 32472.47	17432.34
	y²F°	0.004	0.003	0.57	0.001	0.0005	0.09
	39926.83	19034.95	2573.91 38839.62	3232.28 30929.14	2853.93 35029.23	2518.06 39701.36	4053.84 24661.23
	z²F°	0.001	0.002	0.23	0.02	0.02	0.0000
	31207.44	10315.56	3319.08 30120.23	4501.27 22209.75	3799.78 26309.84	3226.76 30981.97	15941.84
	x²F°	0.01	0.0000	0.0000	0.0000	0.0000	2.04
	47625.17	3739.50 26733.29	46537.96	38627.48	42727.57	47399.70	3089.40 32359.57
	z ⁴ F°	0.0000	0.11	0.009	0.004	0.32	0.0000
	30958.70	10066.82	3346.73 29871.49	21961.01	3836.10 26061.10	3252.91 30733.23	15693.10
	z4G°	0.0000	0.0005	0.0006	0.0002	0.009	0.0000
0	29544.37	8652.49	3513.08 28457.16	4865.62 20546.68	4056.20 24646.77	3409.81 29318.90	14278.77
l							

 $(3d^24p)$

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TABLE 1.—Continued

		1	T		T	
7/2	$b^2\mathrm{F}$	b ⁴ F	a ² G	$a^2\mathrm{F}$	a ⁴ F	$b^2\mathrm{G}$
7/2	20891.88	1087.21	8997.69	4897.60	225.47	15265.6
y ⁴ D°	0.003	0.03 2517.43	0.001	0.005 2784.67	0.004 2464.00	0.0001
40798.37	19906.49	39711.16	31800.68	35900.77	40572.90	25532.77
z ⁴ D°	0.0004	0.07 3155.67	0.0000	0.006 3587.13	0.24 3072.11	0.0000
32767.02	11875.14	31679.81	23769.33	27869.42	32451.55	17501.42
y²F°	0.10 5211.58	0.002	0.03	0.17 2841.94	0.0002	0.002
40074.71	19182.83	38987.50	31077.02	35177.11	39849.24	24809.11
$z^2\mathrm{F}^\circ$	0.17	0.02 3288.13	0.007 4444.56	2.21 3759.30	0.04 3197.52	0.001
31490.82	10598.94	30403.61	22493.13	26593.22	31265.35	16225.22
x ² F°	0.36 3761.89	0.0000	0.01	0.01	0.0000	0.08 3104.60
47466.80	26574.92	46379.59	38469.11	42569.20	47241.33	32201.20
z ⁴ F°	0.005	0.58 3329.46	0.0001	0.05 3813.39	2.04 3236.57	0.0000
31113.61	10221.73	30026.40	22115.92	26216.01	30888.14	15848.01
z²G°	0.0004	0.0001	0.31 3913.46	0.09 3372.21	0.0005 2913.08	0.18 5185.90
34543.36	13651.48	33456.15	25545.67	29645.76	34317.89	19277.76
y ² G°	0.003	0.0000	0.008 2877.44	0.005 2573.72	0.0000	2.63 3510.84
43740.77	22848.89	42653.56	34743.08	38843.17	43515.30	28475.17
z ⁴ G°	0.0002	0.02 3489.74	0.0001	0.003 4025.14	0.33 3387.84	0.0000
29734.45	8842.57	28647.24	20736.76	24836.85	29508.98	14468.85

TABLE 1.—Continued

7/2	$b^2\mathrm{F}$	b ⁴ F	a ² G	a^2 F	a ⁴ F	b ² G
9/2, 11/2	20891.88	1087.21	8997.69	4897.60	225.47	15265.6
z ⁴ F°	0.0000	0.09	0.0000	0.002	0.24	0.0000
31300.92	10409.04	3308.81 30213.71	22303.23	26403.32	3217.06 31075.45	16035.32
z ² G°	0.04	0.0000	0.01	3.16	0.0001	0.0007
34748.50	13856.62	33661.29	25750.81	3349.04 29850.90	2895.81 34523.03	19482.90
y ² G°	0.25	0.0000	0.01 2874.08	0.10 2571.03	0.0000	0.05
43780.99	4367.66 22889.11	42693.78	34783.30	38883.39	43555.52	28515.39
z4G°	0.0000	0.10 3461.50	0.0000	0.0000	3.09 3361.21	0.0000
29968.08	9076.20	28880.87	20970.39	25070.48	29742.61	14702.48
$z^2 \mathrm{H}^\circ$	0.0001	0.0000	0.02 2725.78	0.0000	0.0000	3.30 3287.66
45673.75	24781.87	44586.54	36676.06	40776.15	45448.28	30408.15

 $(3d^{2}4p)$

TABLE 1.—Continued

		A CONTRACTOR OF THE PARTY OF TH	120000000000000000000000000000000000000		
9/2, 11/2	b⁴F	a ² G	$a^2\mathrm{H}$	a ⁴ F	b ² G
7/2	1215.58	9118.15	12676.99	393.22	15257.53
y ⁴ D°	0.28 2525.60	0.03	0.0000	0.04 2474.22	0.006
40798.37	39582.79	31680.22	28121.38	40405.15	25540.84
z ⁴ D°	0.56	0.0007	0.0000	2.36	0.0000
32767.02	3168.52 31551.44	23648.87	20090.03	3088.02 32373.80	17509.49
y ² F°	0.01	0.70	0.002	0.003	0.12
40074.71	38859.13	3229.42 30956.56	3648.87 27397.72	2519.31 39681.49	4028.34 24817.18
z²F°	0.0001	0.30	0.0001	0.02	0.0000
31490.82	3302.09 30275.24	4468.50 22372.67	18813.83	3214.75 31097.60	16233.29
x ² F°	0.0000	0.0000	0.0001	0.0000	2.63
47466.80	46251.22	38348.65	34789.81	47073.58	3103.80 32209.27
z ⁴ F°	0.09	0.009	0.0001	0.24	0.0000
31113.61	3343.77 29898.03	4545.14 21995.46	18436.62	3254.25 30720.39	15856.08
z2G°	0.0000	0.03	0.66	0.0000	0.001
34543.36	33327.78	3932.02 25425.21	4571.98 21866.37	34150.14	5183.73 19285.83
y ² G°	0.0000	0.01	0.90	0.0000	0.06
43740.77	42525.19	2887.46 34622.62	3218.27 31063.78	43347.55	3509.85 28483.24
z4G°	0.0005	0.0002	0.0003	0.006	0.0000
29734.45	28518,87	20616.30	17057.46	3407.20 29341.23	14476.92

TABLE 1. - Concluded

 $(3d^3 + 3d^24s)$

			-	_		·	
$(3d^24p)$	9/2, 11/2 9/2,	b⁴F	a ² G	$a^2\mathrm{H}$	a ⁴ F	$b^2\mathrm{G}$	$a^2\mathrm{H}$
	11/2	1215.58	9118.15	12676.99	393.22	15257.53	12774.81
	z ⁴ F° 31300.92	0.91 3322.94 30085.34	0.0001 22182.77	0.0000 18623.93	3.10 3234.52 30907.70	0.0004 16043.39	0.0001 18526.11
	z ² G° 34748.50	0.0005 33532.92	0.38 3900.54 25630.35	0.02 4529.46 22071.51	0.003 2909.92 34355.28	0.24 5129.15 19490.97	0.81 4549.63 21973.69
	y ² G° 43780.99	0.0000 42565.41	0.01 2884.11 34662.84	0.03 3214.12 31104.00	0.0000 43387.77	3.33 3504.89 28523.46	1.09 3224.24 31006.18
	z ⁴ G° 29968.08	0.01 3476.99 28752.50	0.0000 20849.93	0.0000 17291.09	0.35 3380.28 29574.86	0.0000 14710.55	0.30 17193.27
	z ² H° 45673.75	0.0000 44458.17	0.004 36555.60	0.0000 3029.73 32996.76	0.0009 45280.53	0.05 3286.78 30416.22	0.009 3038.71 32898.94
	z ⁴ G° 30240.68	0.13 3444.31 29025.10	0.0000 21122.53	0.0000 17563.69	4.00 3349.41 29847.46	0.0000 14983.15	0.0000 17465.87
	z ² H° 45908.56	0.0000 44692.98	0.02 2717.29 36790.41	0.01 3008.33 33231.57	0.0000 45515.34	4.02 3261.60 30651.03	0.47 3017.19 33133.75

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